11) The third sentence of the first paragraph on p. 1109 should read "For the FD case, the best efficiency is only 4.8% with $Z_{\rm cpw} = 9.5\ \Omega$, $f_{c,\rm ls}/f_B = 4$ leading to $\Delta z = 1.145\ \mu$m (simulation step), and $L_{\rm FD} = 800\ \mu$m (the length $L_{\rm FD}$ was varied over 100-μm steps)."
12) The eighth sentence of the first paragraph on p. 1110 should read "If W is increased without increasing S, $Z_{\rm cpw}$ decreases, leading to a decrease of $Z_{\rm ls}$, and then a mismatched NLTL."
13) The sixth sentence of Section III-C on p. 1111 should read "To bring to the fore the importance of the mismatch between $Z_{\rm ls}$ and the load and source impedances, two sets of simulations were carried out for FD NLTLs, first using 50-Ω source and load impedances, meaning that the NLTL is strongly mismatched, and, second, with the source and load impedances made equal to $Z_{\rm ls}$."
14) The following paragraph should be inserted following the third paragraph on p. 1113 "Fig. 23 compares the measured results with SPICE simulations of the two NLTLs when biased to −6 V and fed by a 12-V peak–peak sinewave. Measurements were done using a Tektronix CSA 803 sampling oscilloscope."
15) The fourth sentence of the first paragraph on p. 1114 should read "We see that $|S_{21}|$ rapidly decreases for frequencies above 1200 and 2200 MHz, respectively."
16) The correct form of second equation on p. 1114 is

$$\mathrm{BW_{ds}} = \frac{\frac{f_B}{3} - \frac{f_B}{5}}{\frac{f_B}{3} + \frac{f_B}{5}}.2 = \frac{1}{2} \equiv 50\%.$$

17) The second paragraph on p. 1115 should read "The waveform in Fig. 5(b) is the solution of the generalized van der Pol (GvdP) oscillator ordinary differential equation (ODE)

$$\frac{d^2y}{dt^2} - \frac{d}{dt}(ay - by^3) + y = 0$$

using $a = 7$, $b = 4$. Here, the cubic is

$$f(y) = -ay + by^3$$

and the solution was obtained using the 'ode15s' stiff ODE solver of MATLAB Release 12."

REFERENCES

[1] J.-M. Duchamp, P. Ferrari, M. Fernandez, A. Jrad, X. Mélique, J. Tao, S. Arscott, D. Lippins, and R. G. Harrison, "Comparison of fully distributed and periodically loaded nonlinear transmission lines," *IEEE Trans. Microwave Theory Tech.*, vol. 51, pp. 1105–1116, Apr. 2003.

Corrections to "Complex Permittivity Measurements of Common Plastics Over Variable Temperatures"

Bill Riddle, James Baker-Jarvis, and Jerzy Krupka

Despite our best efforts to present error-free measurements to the IEEE Microwave Theory and Techniques Society (IEEE MTT-S), one of the figures in the above paper [1] contains an incorrect scaling factor. In [1, Fig. 11], the loss tangent data for polycarbonate is low by a factor of ten. The correct data is shown in Fig. 1 in this paper. We apologize for any confusion this error may have caused.

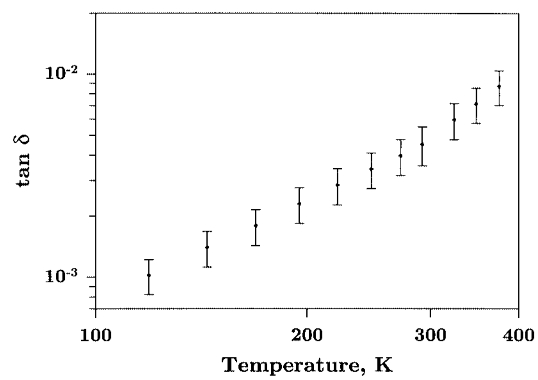

Fig. 1. Polycarbonate, $f \approx 11$ GHz, loss tangent versus temperature.

REFERENCES

[1] B. Riddle, J. Baker-Jarvis, and J. Krupka, "Complex permittivity measurements of common plastics over variable temperatures," *IEEE Trans. Microwave Theory Tech.*, vol. 51, pp. 727–733, Mar. 2003.

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B. Riddle and J. Baker-Jarvis are with the Radio-Frequency Technology Division, National Institute of Standards and Technology, Boulder, CO 80305-3328 USA (e-mail: Bill.Riddle@nist.gov).
J. Krupka is with the Institute of Microelectronics and Optoelectronics, Warsaw University of Technology, Warsaw 00-662, Poland.
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